

TYPE 460 : HYPOCAUST (AIR-TO-SOIL EXCHANGER)**General Description**

This component models an air-to-soil heat exchanger. It accounts for sensible as well as latent exchanges between airflow and tubes, diffusion into surrounding soil, frictional losses and flow of condensed water along the tubes. Local heating from integrated fan motor can be taken into account at tube inlet or outlet. Direction of airflow can be controlled (stratification in case of heat storage) and flexible geometry allows for inhomogeneous soils as well as diverse border conditions.

Nomenclature

List hereafter covers all symbols used in the mathematical description of the model (other symbols are defined directly in the component configuration section). When as here, symbols in text account for currently described node and timestep, while subscripts are used to reference neighbour nodes or previous timestep.

<i>ClatWat</i>	Latent heat of water
<i>CmAir</i>	Mass-specific heat of air
<i>CmVap</i>	Mass-specific heat of vapour
<i>CmWat</i>	Volume-specific heat of water
<i>CvSoil</i>	Volume-specific heat of soil
<i>CvTub</i>	Volume-specific heat of tube
<i>Ctub</i>	Circumference of tube
<i>Dt</i>	Internal timestep
<i>Dl</i>	Node width (along x, y or z)
<i>Dtub</i>	Hydraulic diameter of tube
<i>Fair</i>	Airflow in tube
<i>FairTot</i>	Airflow, total (over tubes and modules)
<i>Hrel</i>	Relative humidity
<i>Hrat</i>	Absolute humidity (vapour pressure)
<i>Hsat</i>	Absolute humidity (vapour pressure) at saturation
<i>Kair</i>	Air/tube exchange coefficient
<i>Kbord</i>	Heat conduction coefficient of border (pondered, including <i>Rsurf</i>)
<i>Ksoil</i>	Heat conduction coefficient to neighbour node or surface (including <i>Rsurf</i>)
<i>LamSoil</i>	Heat conductivity of soil
<i>LamTub</i>	Heat conductivity of tube
<i>MmolAir</i>	Molar mass of air
<i>MmolWat</i>	Molar mass of water
<i>Mair</i>	Mass of air exchanged between airflow and tube superficial layer
<i>Mwat</i>	Mass of free water
<i>MwatIn</i>	Mass of water flowing into node
<i>MwatInf</i>	Mass of water infiltrating into node

<i>MwatLat</i>	Mass of water cond./evap.
<i>MwatOut</i>	Mass of water flowing or ejected out of node
<i>Pfric</i>	Energy rate of frictional losses
<i>Pint</i>	Energy rate of tube or soil internal gains
<i>Plat</i>	Energy rate of latent air-tube heat exchange
<i>Psbl</i>	Energy rate of sensible air-tube heat exchange
<i>Psoil</i>	Energy rate of heat diffused by neighbour nodes
<i>Pwat</i>	Energy rate of free water internal losses
<i>PrAir</i>	Pressure of air
<i>Rsurf</i>	Surface heat resistance
<i>Rfric</i>	Friction coefficient of tubes
<i>RhoAir</i>	Specific weight of air
<i>Sair</i>	Section of tube
<i>Sbord</i>	Area of border
<i>Ssoil</i>	Lateral area of soil node
<i>Stub</i>	Lateral area of tube node
<i>Tair</i>	Temperature of air
<i>Tbord</i>	Pondered temperature of border
<i>Tsoil</i>	Temperature of soil
<i>Ttub</i>	Temperature of tube
<i>ThTub</i>	Thickness of tube
<i>Vair</i>	Air velocity
<i>Vwat</i>	Velocity of water
<i>VolSoil</i>	Node volume
<i>VolTub</i>	Volume of tube node
<i>Hrat</i>	Humidity ratio

Mathematical Description

Geometry

The model describes a block of rectangular soil nodes (which need not all share same physical properties), comprising parallel tubes that run along the x-axis (see figure 1). A correction factor allows to describe non-rectangular tubes. If not adiabatic, surface conditions (which need not expand from edge to edge) can be given in terms of either inflowing energy rate or temperature. An additional surface resistance can be defined, especially for direct coupling with air temperature.

For matter of simplification and run time economy, symmetries in the y-z plane can be used by describing only one module (=relevant part) and specifying the number of times it is used. In this case the symmetry surface(s), which must be subject to adiabatic condition, may if necessary pass through the middle of some tubes (see figure 1).

Parameterisation of chosen geometry occurs in following way (of which best understanding can be taken from figure 1 and example at end) :

- define the occurrence of typical cross-sections along the x-axis, with numbers that refer to them.
- define the typical cross-sections in the y-z plane, with numbers that refer to soil types, respectively surface conditions.
- define two additional cross-sections for frontal and rear surface conditions.

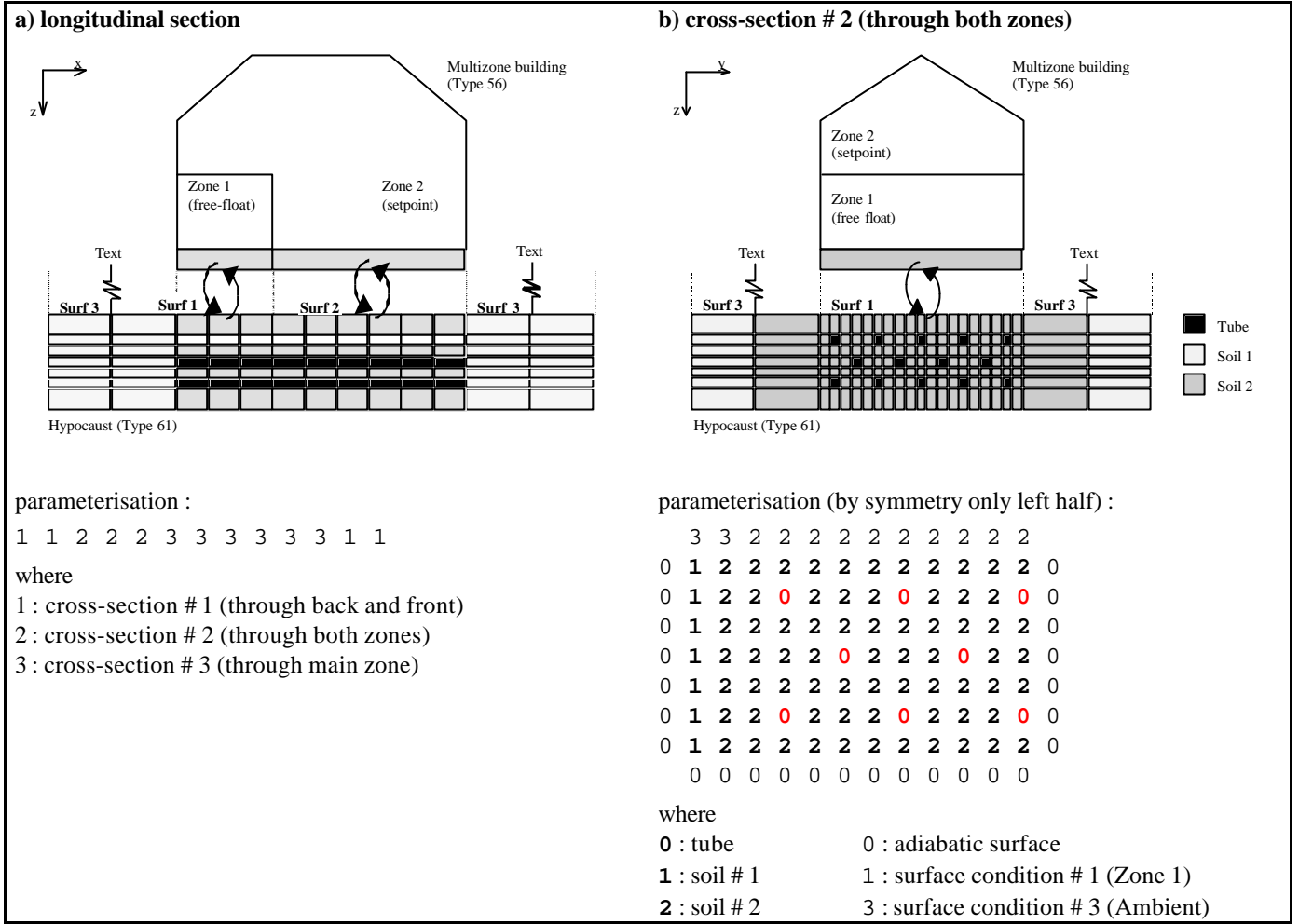


Fig.1 : Example of Type460 geometry and coupling to other Type.

Linking

In addition to airflow at inlet/outlet, surface conditions can also be coupled to other Types. One can therefore choose between following two modes :

- If output from other module (=input for Type 460) is the energy rate flowing into hypocaust, Type460 will return equivalent border temperature as output (=input for other Type). Latter is defined as the pondered average node temperature of all nodes comprised in that particular surface :

$$T_{bord} = \frac{\sum_{i \in bord} S_{soil_i} \cdot K_{soil_i} \cdot T_{soil_i}}{S_{bord} \cdot K_{bord}} \tag{1}$$

with

$$K_{soil_i} = \frac{1}{\frac{Dl_i/2}{Lam_{Soil_i}} + R_{surf}}$$

$$S_{bord} = \sum_{i \in bord} S_{soil_i}$$

$$K_{bord} = \frac{\sum_{i \in bord} S_{soil_i} \cdot K_{soil_i}}{S_{bord}}$$

One has to take care to use identical border area S_{bord} and heat conduction coefficient K_{bord} in other Type (check these calculated values in parameter control file). The timestep iteration procedure of TRNSYS then will guarantee for proper energy balance (energy rate flowing out of one module = energy rate flowing into other module), which can be checked by plotting inflowing energy rate as optional output of Type 460.

- If on the contrary output from other module is its equivalent border temperature, Type460 will return inflowing energy rate as output. Proper energy balance again is guaranteed by using identical border area and heat conduction coefficient in both Types.

Air flow

Air flow is either positive, negative or zero. If modelling a set of tubes of distinct cross sections, total flow is distributed among the tubes in following way :

$$Fair = FairTot \cdot \frac{S_{air} \cdot \sqrt{Dtub}}{\sum_{tubes} (S_{air} \cdot \sqrt{Dtub})} \quad (2)$$

so that according to form of pressure losses (see equation 12 further on) pressure equilibrium at output as well as power and flow integrals are respected.

Water flow

Apart from condensation of airflow (see air-tube heat exchange, further on), water can also enter tubes by infiltration (along part or all of the tube surface). Resultant free water either flows along the tubes or is directly ejected out of hypocaust (flow/ejection occurs in same direction than airflow, in positive direction when airflow is zero). Water flowing/ejected out of a tube node is :

$$M_{watOut} = \begin{cases} \left(M_{wat_{t-1}} + \Delta M_{wat} \right) \frac{V_{wat} \cdot Dt}{Dl} & \text{if water is flowing} \\ \left(M_{wat_{t-1}} + \Delta M_{wat} \right) & \text{if water is ejected} \end{cases} \quad (3)$$

where

$$\Delta M_{wat} = M_{watIn} + M_{watInf} + M_{watLat}$$

while water flowing from preceding node ($i \pm 1$, depending on flow direction) into actual one is :

$$M_{watIn} = \begin{cases} M_{watOut_{i \pm 1}} & \text{if water is flowing} \\ 0 & \text{if water is ejected} \end{cases} \quad (4)$$

Air-tube heat exchange

In each tube node, from inlet towards outlet, following heat exchanges are taken into account :

- **Sensible heat** is characterised by a an exchange coefficient which depends on flowrate. Cutting short on dimensionless analysis, the model uses a linear dependence on air velocity (as derived from experiences on large plane surfaces [3] and confirmed by the author in the frame of an experience on a buried pipe system).

$$K_{air} = K_{air0} + K_{air1} \cdot V_{air} \quad (5)$$

so that

$$P_{sbl} = Stub \cdot K_{air} \cdot (T_{air} - T_{tub}) \quad (6)$$

- **Latent heat** is determined by the Lewis approach [4] which considers proceeding sensible heat exchange to result from an air mass exchange between the airflow and a superficial air layer on the tube surface, at latters temperature and saturated in humidity. Analogy between heat and mass transfer readily give exchanged air mass during timestep Dt :

$$M_{air} = \frac{P_{sbl} \cdot Dt}{C_{mAir} \cdot (T_{air} - T_{tub})} \quad ,$$

that is

$$M_{air} = \frac{Stub \cdot K_{air} \cdot Dt}{C_{mAir}} \quad . \quad (7)$$

This air exchange conveys a vapour transfer, which is determined by the difference of humidity ratios of the airflow and the saturated layer :

$$\begin{aligned} M_{watLat} &= (H_{rat}(T_{air}, H_{rel}) - H_{rat}(T_{tub}, 100\%)) \cdot M_{air} \\ &= (H_{rat}(T_{air}, H_{rel}) - H_{rat}(T_{tub}, 100\%)) \cdot \frac{Stub \cdot K_{air} \cdot Dt}{C_{mAir}} \end{aligned} \quad (8)$$

where, from equation of perfect gazes, humidity ratio computes as

$$H_{rat}(T, H_{rel}) = \frac{H_{sat}(T_{air}) \cdot M_{molWat}}{P_{rAir} \cdot M_{molAir}} \quad (9)$$

According to its sign, this vapour transfer corresponds to condensation ($M_{watLat} > 0$) or evaporation ($M_{watLat} < 0$). In latter case M_{watLat} is furthermore limited by 1) available free water in node and 2) saturation pressure of air. Latent heat exchange is finally expressed as

$$P_{lat} = C_{lat} \cdot \frac{M_{watLat}}{Dt} \quad (10)$$

- **Diffused heat** from surrounding nodes (4 soil nodes, 2 tube nodes) is given by

$$P_{soil} = \sum_{i=1}^6 S_{soil_i} \cdot K_{soil_i} \cdot (T_{soil_{i,t-1}} - T_{tub}) \quad (11)$$

where

$$K_{soil_i} = \begin{cases} \frac{1}{\frac{Th_{Tub}}{Lam_{Tub}} + \frac{Dl_i/2}{Lam_{Soil_i}}} & \text{if neighbor is soil} \\ \frac{1}{\frac{Dl/2}{Lam_{Tub}} + \frac{Dl_i/2}{Lam_{Tub}}} & \text{if neighbor is tube} \end{cases}$$

- **Heat from frictional losses** relates to pressure drop along the tubes, which commonly writes [5] as

$$\Delta Pr_{Air} = R_{fric} \cdot \frac{Dl}{Dtub} \cdot \frac{Rho_{Air} \cdot V_{air}^2}{2}$$

or

$$\Delta Pr_{Air} = R_{fric} \cdot \frac{Dl \cdot Rho_{Air}}{2} \cdot \frac{F_{air}^2}{S_{air}^2 \cdot Dtub} \quad (12)$$

where the friction coefficient R_{fric} is here considered to be independent of air velocity, and the hydraulic diameter of the tube writes as

$$Dtub = \frac{4 \cdot S_{air}}{C_{tub}} \quad (13)$$

Related energy rate then writes as

$$P_{fric} = F_{air} \cdot \Delta Pr_{Air} \quad (14)$$

and is supposed to be gained entirely by the airflow (see energy balance further on).

- **Heat lost by free water** computes as

$$P_{wat} = C_m W_{at} \cdot \frac{M_{wat_{t-1}} \cdot (T_{tub_{t-1}} - T_{tub}) + M_{watIn} \cdot (T_{tub_{i\pm i}} - T_{tub})}{Dt} \quad (15)$$

- **Internal heat gain** is the heat gained by the tube :

$$P_{int} = \frac{Cv_{Tub} \cdot Vol_{Tub} \cdot (T_{tub} - T_{tub_{t-1}})}{Dt} \quad (16)$$

Preceding energy rates allow to calculate new tube temperature and free water content of actual node, as well as air temperature and humidity ratio of next node. Since the saturated humidity in (9) is non-linear in terms of temperature, T_{tub} is determined by numerical resolution of the tube energy balance

$$P_{int} = P_{sbl} + P_{lat} + P_{soil} + P_{wat} \quad , \quad (17)$$

while water balance readily yields

$$M_{wat} = M_{wat_{t-1}} + M_{watLat} + M_{watInf} + M_{watIn} - M_{watOut} \quad . \quad (18)$$

Sensible energy and water balance on air finally yield air conditions of next node ($i \pm 1$) :

$$T_{air_{i \pm 1}} = T_{air} + \frac{P_{fric} - P_{sbl}}{(Cm_{Air} + H_{rat} \cdot Cm_{Vap}) \cdot Rho_{Air} \cdot S_{air} \cdot V_{air}} \quad , \quad (19)$$

$$H_{rat_{i \pm 1}} = H_{rat} - \frac{M_{watLat}}{Rho_{Air} \cdot S_{air} \cdot V_{air} \cdot Dt} \quad , \quad (20)$$

where calculation can be pursued in same manner.

Soil-soil, soil-tube and soil-surface exchanges

Dynamic of soil nodes relies on diffusive heat from neighbour nodes :

$$P_{soil} = \sum_{i=1}^6 S_{soil_i} \cdot K_{soil_i} (T_i - T_{soil_{t-1}}) \quad , \quad (21)$$

where

$$T_i = \begin{cases} T_{soil_{i,t-1}} & \text{if neighbor is soil} \\ T_{tub_{i,t}} & \text{if neighbor is tube} \\ T_{surf_{i,t}} & \text{if neighbor is surface} \end{cases}$$

and

$$K_{soil_i} = \begin{cases} \frac{1}{\frac{Dl/2}{LamSoil} + \frac{Dl_i/2}{LamSoil}} & \text{if neighbor is soil} \\ \frac{1}{\frac{Dl/2}{LamSoil} + \frac{ThTub}{LamTub}} & \text{if neighbor is tube} \\ \frac{1}{\frac{Dl/2}{LamSoil} + R_{surf}} & \text{if neighbor is surface} \end{cases}$$

It allows to compute new soil temperature :

$$T_{soil} = T_{soil_{t-1}} + \frac{P_{soil}}{CvSoil \cdot VolSoil} \quad . \quad (22)$$

Initialisation

Hypocaust is initialised with a common initial temperature for all nodes, as well as a common initial water thickness along all tubes. Optionally one may define additional initial temperatures and water thickness for certain nodes or node clusters (see further on, definition of parameter file).

TRNSYS Component Configuration

Source code is separated into two files :

- **Type460.for** contains actual routine and is organised in different subroutines.
- **Type460.inc** is an include file used by the subroutines. It contains definition of variables and their organisation in common blocks, as well as definition of maximum allowed sizes, which are listed hereafter with their default values :

<i>NIMax</i>	max number of nodes along x	40
<i>NJMax</i>	max number of nodes along y (per module)	100 ¹⁾
<i>NKMax</i>	max number of nodes along z (per module)	20 ¹⁾
<i>NtubMax</i>	max number of tubes (per module)	20 ¹⁾
<i>NsoilMax</i>	max number of soiltypes	10
<i>NsurfMax</i>	max number of surfaces	6 ²⁾
<i>NoptMax</i>	max number of optional outputs	100 ²⁾
<i>NiniMax</i>	max number of initialisation conditions	20

1) module = relevant part in y-z plane (see further up, description of geometry).

2) Changing default values for maximum number of surfaces or maximum number of optional outputs will need re-numeration of routine arguments (parameters, inputs and outputs) as defined in information flow diagram.

Input data is separated into three groups, of which two are passed as arguments, the last one read from a file :

- **Parameters** describe fixed data that deal with linking to other modules and with simulation deck.
- **Inputs** describe variable data.
- Parameters which are proper to the model are passed by means of a **Parameter definition file**, which is read by the routine at initialisation. While reading, the data is checked and rewritten to a control file (see below), so that eventual errors can be tracked.

Output data is separated into two groups, of which first one is returned as argument, second one written to a file :

- **Outputs** describe variable data, which can be linked to other modules.
- Parameters which are derived from supplied parameter file or from simulation deck are written to a **Parameter control file**, which can be used to check for proper definition. As pointed out, first part of this file is a formatted and commented copy of Parameter definition file (which it can substitute).

A synoptic view of these data groups is to be found in the information flow diagram (next section), while this section presents each of them in a detailed table (with explanatory notes following last table).

Note, especially in case of debugging, that data is passed to/from the routine with TRNSYS compatible units as defined hereafter, where it is converted to standard SI units.

Parameters

Number	Symbol	Definition and unit	
1	<i>IparDef</i>	Logical unit of Parameter definition file [-]	1)
2	<i>IparCon</i>	Logical unit of Parameter control file [-]	1)
3	<i>Dt</i>	Internal time step [hr]	2)
4	<i>FairMin</i>	Minimum airflow [m ³ /hr]	3)
5	<i>DTtubTol</i>	Temperature tolerance for tube energy balance [K]	4)
6 - 11	<i>TypSurf</i>	Linking modes for surfaces 1 - 6 [-]	5)
12 - 17	<i>Rsurf</i>	Heat resistance at surfaces 1 - 6 [K m ² hr/kJ]	

Inputs

Number	Symbol	Definition and unit	
1	<i>FairTot</i>	Airflow, total over all modules [m ³ /hr]	6)
2	<i>TairIn</i>	Inlet temperature [°C]	
3	<i>HrelIn</i>	Inlet relative humidity [%]	
4	<i>PrAir</i>	Air pressure [bar]	7)
5	<i>FwatInfTot</i>	Water infiltration, total over all modules [m ³ /hr]	8)
6 - 11	<i>Xsurf</i>	Surface conditions for surfaces 1 - 6 [°C] or [kJ/hr]	5)

Parameter definition file

Each data set hereafter is written on one line (exception for *TypSoil* arrays, which take *NK* or *NK+2* lines). Data within one dataset is separated by commas or blanks. Comments can be entered by using an asterix (*) in first column.

Symbol	Definition and unit	
<i>Nmod,Nsec,Nsoil,Nsurf,NI,NJ,NK</i>	Number of : modules, cross-sections, surfaces, nodes along x-axis, nodes along y-axis, nodes along z-axis [-]	
<i>Dx (1:NI)</i>	Node width along x-axis [m]	9)
<i>Dy (1:NJ)</i>	Node width along y-axis [m]	9)
<i>Dz (1:NK)</i>	Node width along z-axis [m]	9)
<i>TypSec(1:NI)</i>	Type of used cross-sections along x-axis [-]	10)
<i>TypSoil (1:NJ,1:NK)</i>	Type of surfaces on frontal cross-section [-]	11)
<i>TypSoil (0:NJ+1,0:NK+1)</i>	Type of soils/surfaces for typical cross-section in y-z plane [-]	12)
<i>TypSoil (1:NJ,1:NK)</i>	Type of surfaces on rear cross-section [-]	11)
<i>PosInf</i>	Position of water infiltration [-]	8)
<i>Kair0, Kair1</i>	Air-tube exchange coefficients [kJ/hr K m ²] and [(kJ/hr K m ²)/(m/s)]	13)
<i>LamSoil, CvSoil</i>	Soil conductivity [kJ/hr K m] and capacity [kJ/K m ³]	14)
<i>LamTub, CvTub</i>	Tube conductivity [kJ/hr K m] and capacity [kJ/K m ³]	
<i>ThTub, CtubCor, Rfric</i>	Tube thickness [m], circumference correction factor [-] and friction coefficient [-]	9) 15)
<i>TypWatFlow (-1:1)</i>	Type of water flow [-]	16)
<i>Vwat (-1:1)</i>	Velocity of water flow [m/hr]	16)
<i>NiniSoil, NiniWat</i>	Number of initial conditions (soil temperatures and water thickness) [-]	17)
<i>TiniSoil, PosIniSoil (1:6)</i>	Initial temperature [°C] and corresponding node position [-]	17)
<i>ThIniWat, PosIniWat (1:6)</i>	Initial water thickness [m] and corresponding node position [-]	17)
<i>Nopt</i>	Number of optional outputs	20)
<i>TypOpt, PosOpt (1:6)</i>	Type of optional output [-] and corresponding node position [-]	20)

Outputs

Number	Symbol	Definition and unit
1	<i>TairOut</i>	Outlet temperature [°C]
2	<i>HrelOut</i>	Outlet relative humidity [%]
3	<i>PsbITot</i>	Sensible energy rate lost by airflow, total over tubes and modules [kJ/hr]
4	<i>PlatTot</i>	Latent energy rate lost by airflow, total over tubes and

5 - 10	<i>Xbord</i>	modules [kJ/hr] Equivalent border output for surfaces 1 - 6 [°C] or [kJ/hr]	5)
11 - 20	<i>Xopt</i>	Optional outputs	20)

Parameter control file

Data hereafter is written at end of file, after formatted copy of Parameter definition file.

Symbol	Definition and unit	
<i>Ntub</i>	Number of tubes (per module) [-]	
<i>IflowIni</i>	Node index of tube start along x-axis [-]	
<i>IflowEnd</i>	Node index of tube end along x-axis [-]	
<i>PosTub(1:2)</i>	Node index of tube position along y- and z-axis [-]	18)
<i>Lx</i>	Length of hypocaust [m]	
<i>Ly</i>	Width of hypocaust (total over modules) [m]	
<i>Lz</i>	Depth of hypocaust [m]	
<i>Ltub</i>	Length of tubes [m]	
<i>SairTot</i>	Tube cross-section area (total over all tubes and modules) [m ²]	
<i>StubTot</i>	Tube surface (total over all tubes and modules) [m ²]	
<i>ZairTot</i>	Normalisation factor for airflow distribution [m ⁵ /2]	
<i>SinfTot</i>	Water infiltration surface, total over all modules [m ²]	8)
<i>Sbord</i>	Border area (total over all modules) [m ²]	19)
<i>Kbord</i>	Equivalent border conduction coefficient [kJ/hr K m ²]	19)
<i>DtSoil</i>	Maximum internal timestep for stability of soil temperature [hr]	
<i>DtWat</i>	Maximum internal timestep for consistency of water flow [hr]	
<i>FairMinTub</i>	Minimum air flow for stability of air temperature [m ³ /hr]	
<i>Dt</i>	Internal timestep effectively used in simulation [hr]	
<i>FairMin</i>	Minimum air effectively flow used in simulation [m ³ /hr]	

Explanatory notes for proceeding tables

- 1) Unless assigned in simulation deck with user-defined name, parameter definition and control files must by default be named ParamDef.txt and ParamCon.txt.
- 2) Since calculation of soil temperature is of explicit type, internal timestep should not exceed a maximum theoretical value *DtSoil*, which is proportional to smallest node volume of soil (problem of temperature oscillation). Consistency of water flow calculation (equation 3) also implies a maximum value *DtWat* for internal timestep, proportional to shortest tube node. Both of these computed values are written to the parameter control file. Type 460 usually takes the smallest of these two values for the internal timestep (which happens by setting the 3rd routine parameter *Dt* to zero). The user may alternatively control soil temperature oscillation by defining a larger or smaller internal timestep himself (which happens by setting the 3rd routine parameter *Dt* to a positive value), in which case the value *DtWat* should not be exceeded though.

- 3) So as to avoid oscillations of air temperature along the tube, airflow should not exceed a theoretical minimum value $FairMinTub$, which is written to the parameter control file. Type 460 usually takes this value as a lower limit to the airflow (which happens by setting the 4th routine parameter $FairMin$ to zero). The user may alternatively control air temperature oscillation by defining a larger or smaller minimum airflow himself (which happens by setting the 4th routine parameter $FairMin$ to a positive value). In both cases an airflow smaller than the minimum value will be set to zero (no air-tube exchange, only diffusion within soil).
- 4) Temperature tolerance (>0) sets precision of numerical resolution of energy balance in tube (equation 17).
- 5) For each surface, linking mode is one of the following :
 0 : corresponding input $Xsurf$ is surface temperature, output $Xbord$ is inflowing energy rate.
 1 : corresponding input $Xsurf$ is inflowing energy rate, output $Xbord$ is equivalent border temperature.
- 6) Airflow direction along x-axis is carried by sign of airflow. If airflow is smaller (in absolute value) than minimum airflow $FairMin$ (see parameter control file) it is considered as zero (no air-tube exchange, only diffusion within soil).
- 7) Air pressure is used to convert volume flow in mass flow as well as to determine humidity ratio from relative humidity (equation 9). In usual cases its dynamic is not known and it is suggested to take standard atmospheric pressure at local altitude, which can be approximated by :

$$PrAir = PrAir_0 \exp(-h/h_0) \text{ with } PrAir_0 = 1.01325 \text{ bar, } h_0 = 7656 \text{ m.}$$

- 8) Water infiltration is distributed on a certain tube area $SinfTot$, defined by the rectangular node cluster $PosInf$ on which infiltration is to take place.
 $PosInf(1)$ and $PosInf(4)$ are lower and upper node index along x-axis.
 $PosInf(2)$ and $PosInf(5)$ are lower and upper node index along y-axis.
 $PosInf(3)$ and $PosInf(6)$ are lower and upper node index along z-axis.
 Only tube nodes within this cluster are considered for water infiltration.
- 9) Even for non-rectangular tubes, node width must be chosen so that cross-section area is given by $DyDz$. Cross-section perimeter, exchange surfaces and hydraulic diameter will be corrected by tube circumference correction factor $CtubCor$. Latter is defined as the ratio between *real* tube perimeter and *rectangular* tube perimeter $2(Dy + Dz)$. For circular tubes node width has to be chosen so that $Dy = Dz = r\sqrt{p} \cong 1.772r$ and circumference correction factor becomes $\frac{1}{2}\sqrt{p} \cong 0.8862$. In case of a symmetry plane passing in the middle of some tubes (tube node at hypocaust border, with lateral adiabatic condition) one furthermore has to divide Dy by half.
 Generally speaking node widths Dx , Dy and Dz have to be chosen according to given problem, reminding that small soil volumes will lead to small internal timesteps and increase of runtime. Tube thickness $ThTub$ may however be set to zero.
- 10) $TypSec(1:NI)$ are positive integer numbers which refer to further on defined typical cross-sections along x-axis.
- 11) $TypSoil(1:NJ,1:NK)$ are integer numbers which refer to given surface conditions for front and rear of hypocaust module (see example at end).
- 12) $TypSoil(0:NJ+1,0:NK+1)$ are integer numbers which refer to further on defined soil types (bulk) or to given surface conditions (border). Exception are the 4 corners $TypSoil(0,0)$, $TypSoil(NJ+1,0)$, $TypSoil(0,NK+1)$, $TypSoil(NJ+1,NK+1)$ which have no significance and are not defined (see figure 1 and example at end). This data set has to be repeated for the $Nsec$ number of typical cross-sections.

13) Common values for air-tube exchange coefficients [3] are :

K_{air0} : 7 - 11 [kJ/hr K m²]

K_{air1} : 14 - 18 [(kJ/hr K m²)/(m/s)]

14) This line has to be repeated for the N_{soil} number of soils.

15) Typical values for Friction coefficient are 0.01 - 0.02 [-].

16) Specification of water flow is given for all 3 airflow directions (negative, zero, positive).

$TypWatFlow$ indicates whether free water is to flow along the tubes (= 1) or to be ejected out (= 2). V_{wat} (≥ 0) specifies velocity of waterflow (if $TypWatFlow = 1$).

17) Initial temperatures are given for rectangular node clusters, defined by $PosIniSoil$:

$PosIniSoil(1)$ and $PosIniSoil(4)$ are lower and upper node index along x-axis,

$PosIniSoil(2)$ and $PosIniSoil(5)$ are lower and upper node index along y-axis,

$PosIniSoil(3)$ and $PosIniSoil(6)$ are lower and upper node index along z-axis,

except for first initial temperature which is applied to all nodes and thus does not need definition of $PosIniSoil$ (see example at end).

Same structure accounts for initial water thickness. In this case only those nodes within the cluster which do effectively corresponds to tube nodes are taken into account though.

18) This line is repeated for the N_{tub} number of tubes.

19) This line is repeated for the N_{surf} number of surfaces.

20) N_{opt} defines the number of desired optional outputs. For each one of them $TypOpt$ specifies the type of optional output and takes a value from one of the three following tables. $PosOpt$ finally defines the rectangular node cluster for which the optional output is to be considered :

$PosOpt(1)$ and $PosOpt(4)$ are lower and upper node index along x-axis,

$PosOpt(2)$ and $PosOpt(5)$ are lower and upper node index along y-axis,

$PosOpt(3)$ and $PosOpt(6)$ are lower and upper node index along z-axis.

If $TypOpt$ relates to tube/air nodes, only tube nodes within cluster will be considered.

If $TypOpt$ relates to soil nodes, only soil nodes within cluster will be considered.

If $TypOpt$ relates to miscellaneous data, $PosOpt$ is of no significance and should be set to 1.

Optional outputs for tube nodes :

Type	Symbol	Definition and unit	
1	T_{air}	Air temperature [°C]	*
2	H_{rel}	Air relative humidity [%]	*
3	H_{abs}	Air absolute humidity [bar]	*
4	H_{rat}	Air humidity ratio [kg vapour/kg air]	*
5	M_{wat}	Free water in node [m ³]	**
6	$M_{watLat/Dt}$	Water condensing (>0) or evaporating (<0) [m ³ /hr]	**
7	$M_{watIn/Dt}$	Water flowing into node [m ³ /hr]	**
8	$M_{watInf/Dt}$	Water infiltrating into node [m ³ /hr]	**
9	$M_{watOut/Dt}$	Water flowing out of node [m ³ /hr]	**
10	T_{soil}	Tube temperature [°C]	**
11	P_{sbl}	Sensible energy rate from air to tube [kJ/hr]	**
12	P_{lat}	Latent energy rate from air to tube [kJ/hr]	**
13	P_{wat}	Energy rate lost by free water [kJ/hr]	**
14	P_{fric}	Energy rate from frictional losses [kJ/hr]	**
15	$P_{soil(0)}$	Energy rate diffused from all 6 neighbour nodes [kJ/hr]	**
16	$P_{soil(1)}$	Energy rate diffused from previous neighbour node along	**

		x-axis (from surface if border node) [kJ/hr]	
17	<i>Psoil(2)</i>	Energy rate diffused from next neighbour node along x-axis (from surface if border node) [kJ/hr]	**
18	<i>Psoil(3)</i>	Energy rate diffused from previous neighbour node along y-axis (from surface if border node) [kJ/hr]	**
19	<i>Psoil(4)</i>	Energy rate diffused from next neighbour node along y-axis (from surface if border node) [kJ/hr]	**
20	<i>Psoil(5)</i>	Energy rate diffused from previous neighbour node along z-axis (from surface if border node) [kJ/hr]	**
21	<i>Psoil(6)</i>	Energy rate diffused from next neighbour node along z-axis (from surface if border node) [kJ/hr]	**
22	<i>Pint</i>	Energy rate of internal gains [kJ/hr]	**
23	<i>Fair</i>	Air flowrate [m ³ /hr]	*
24	<i>Vair</i>	Air velocity [m/s]	*

* averaged over node cluster

** integrated over node cluster and multiplied by number of modules

Optional outputs for soil nodes :

Type	Symbol	Definition and unit	
101	<i>Tsoil</i>	Soil temperature [°C]	*
102	<i>Psoil(0)</i>	Energy rate diffused from all 6 neighbour nodes [kJ/hr]	**
103	<i>Psoil(1)</i>	Energy rate diffused from previous neighbour node along x-axis (from surface if border node) [kJ/hr]	**
104	<i>Psoil(2)</i>	Energy rate diffused from next neighbour node along x-axis (from surface if border node) [kJ/hr]	**
105	<i>Psoil(3)</i>	Energy rate diffused from previous neighbour node along y-axis (from surface if border node) [kJ/hr]	**
106	<i>Psoil(4)</i>	Energy rate diffused from next neighbour node along y-axis (from surface if border node) [kJ/hr]	**
107	<i>Psoil(5)</i>	Energy rate diffused from previous neighbour node along z-axis (from surface if border node) [kJ/hr]	**
108	<i>Psoil(6)</i>	Energy rate diffused from next neighbour node along z-axis (from surface if border node) [kJ/hr]	**
109	<i>Pint</i>	Energy rate of internal gains [kJ/hr]	**

* averaged over node cluster

** integrated over node cluster and multiplied by number of modules

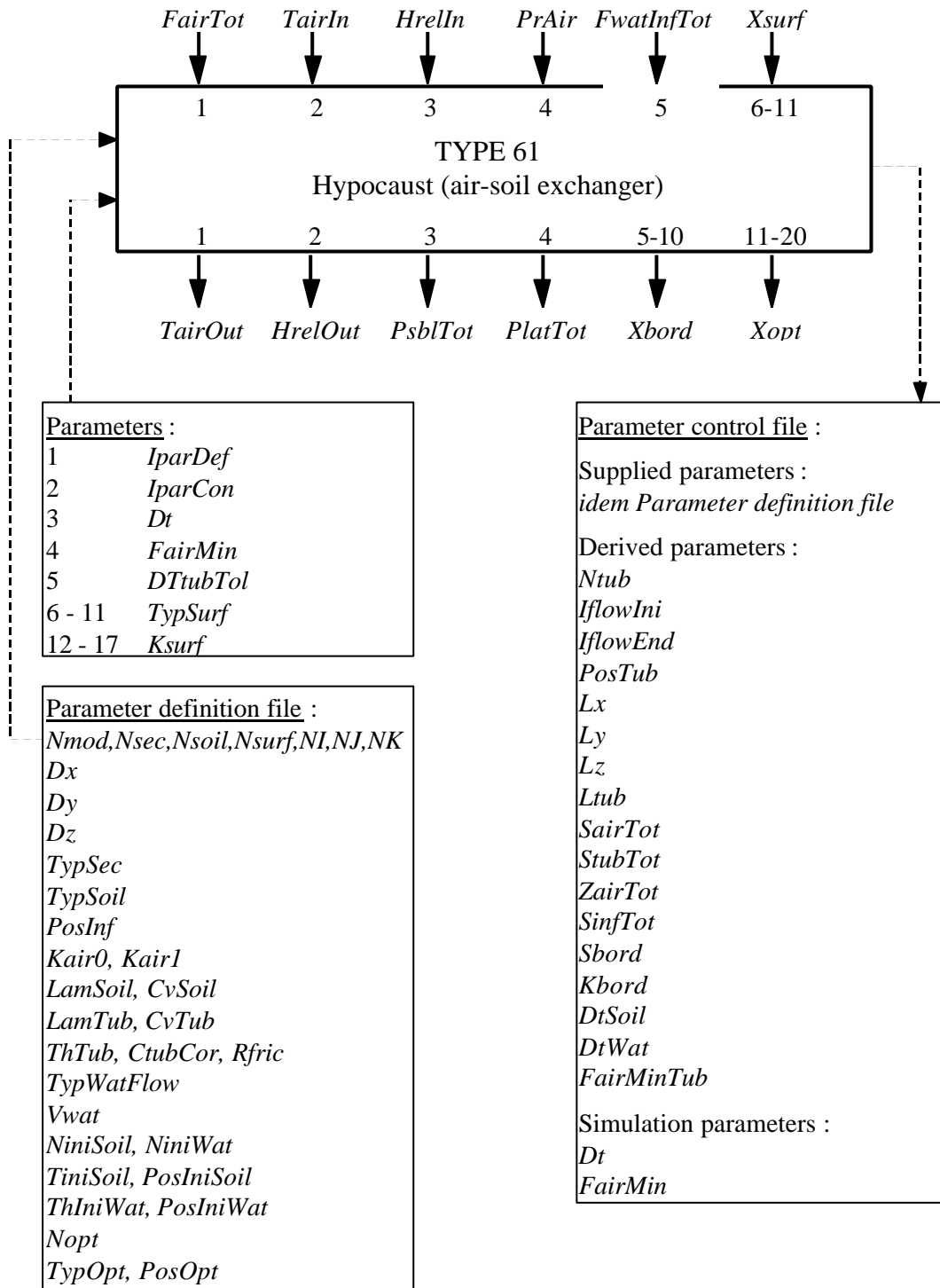
Miscellaneous data for optional output :

Type	Symbol	Definition and unit
201	<i>PsurfTot</i>	Total inflowing energy rate through surfaces (over all modules) [kJ/hr]
202	<i>PwatTot</i>	Total energy loss of free water (over all modules) [kJ/hr]
203	<i>PfricTot</i>	Total frictional losses (over all modules) [kJ/hr]
204	<i>PintTot</i>	Total tube and soil capacitive gains (over all modules) [kJ/hr]

Références

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2. Razafinjohany E., *Etude comparative dans les serres agricoles de deux systèmes de stockage de la chaleur influencé de l'humidité de l'air*, Thèse, 1989, Académie de Montpellier, Université de Perpignan.
3. Molineaux B., Lachal B., and Guisan O., *Thermal analysis of five outdoor swimming pools heated by unglazed solar collectors*, Solar Energy, Vol. 53, Nb. 1, July 1994, pp. 21-26.
4. Incropera F. P., De Witt D. P., *Fundamentals of heat and mass transfer*, John Wiley & Sons Inc., 1990.
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Information Flow Diagram



Example

Description

Example is the underground cooling system shown in Fig. 1. It is a mere case study ment to show the possibility of linking Type460 to the multizone building Type 56 and to check consistency of exchanged energy rates as well as of other internal variables. Hence following hypothesis are made :

- Ambient conditions are constant : temperature of 30°C, humidity of 50%, no solar radiation.
- Building is simplified to its uttermost : a first zone (8 m², 16 m³) with simple brick wall is free-floating and adjoins a second zone (12 m², 39 m³) with insulated brick wall and at fixed temperature (15°C). No windows are taken into account and no infiltration nor cross-ventilation is considered.
- Pipe system is underneath building and laterally not insulated, wherefore lateral and from hypocaust distinct soil is taken into account.
- Airflow is constant (1000 m³/hr) and is not injected into building but supposed to be used elsewhere.
- No water infiltration is considered, nor does free water flow along the tubes.
- Initial temperatures are 10°C for hypocaust, 15°C for surrounding soil and building.

Following variables are defined and analysed (some of which, for checking of proper energy and mass balance, are calculated by two alternative ways defined in the deck) :

<i>Psbl</i>	: sensible energy lost by airflow
<i>Plat</i>	: latent energy lost by airflow
<i>Pin</i>	: internal gains of hypocaust and surrounding soil
<i>PinG, PinG#</i>	: internal gains of surrounding soil
<i>PinH, PinH#</i>	: internal gains of hypocaust
<i>PinHt</i>	: internal gains of hypocaust tubes
<i>PinHs</i>	: internal gains of hypocaust soil
<i>Pfree, Pfree#</i>	: energy diffused from free-floating zone into hypocaust
<i>Pfix, Pfix#</i>	: energy diffused from fixed setpoint zone into hypocaust
<i>Pamb</i>	: energy diffused from ambient into surrounding soil
<i>Pfront</i>	: energy diffused from surrounding soil front of the building into hypocaust
<i>Pback</i>	: energy diffused from surrounding soil back of the building into hypocaust
<i>Pside</i>	: energy diffused from surrounding soil to side of the building into hypocaust
<i>Pwat</i>	: energy diffused from free water into hypocaust
<i>Pfric</i>	: friction losses
<i>T1-T4</i>	: temperatures of airflow along tubes (mean value of all tubes)
<i>Tout</i>	: temperature of airflow at outlet
<i>Tfree</i>	: temperature of free-floating zone, air
<i>TgFree</i>	: temperature of free-floating zone, ground
<i>Tfix</i>	: temperature of fixed setpoint zone, air
<i>TgFree</i>	: temperature of fixed setpoint zone, ground
<i>Mwat, Mwat#</i>	: free water within tubes
<i>dMlat</i>	: condensation/evaporation within tubes
<i>dMout</i>	: total outflowing water.

TYPE 460 : HYPOCAUST (AIR-SOIL EXCHANGER)

Next pages show files for parameterisation of the system (parameter definition file for Type 460, building definition file for Type 56, simulation deck), after which corresponding simulation results are discussed.

Type460.par : parameter definition file (Type 460)

```

*****
* TYPE 460 SUPPLIED PARAMETERS
*=====
* Nmod,Nsec,Nsoil,Nsurf,NI,NJ,NK [-]:
  2   3   2   3   13 12  7

* DX [m]:
  1.0000E+00  1.0000E+00
  0.6666E+00  0.6666E+00  0.6666E+00
  0.6666E+00  0.6666E+00  0.6666E+00
  0.6666E+00  0.6666E+00  0.6666E+00
  1.0000E+00  1.0000E+00

* DY [m]:
  1.0000E+00  1.0000E+00  0.3000E+00  0.2000E+00
  0.2000E+00  0.2000E+00  0.2000E+00  0.2000E+00
  0.2000E+00  0.2000E+00  0.2000E+00  0.1000E+00

* DZ [m]:
  0.4000E+00  0.2000E+00  0.2000E+00  0.2000E+00
  0.2000E+00  0.2000E+00  0.4000E+00

* TypSec [-]:
  1   1   2   2   2   3   3   3   3   3   3   1   1

* TypSoil for front surface [-]:
  0   0   0   0   0   0   0   0   0   0   0   0   0
  0   0   0   0   0   0   0   0   0   0   0   0   0
  0   0   0   0   0   0   0   0   0   0   0   0   0
  0   0   0   0   0   0   0   0   0   0   0   0   0
  0   0   0   0   0   0   0   0   0   0   0   0   0
  0   0   0   0   0   0   0   0   0   0   0   0   0
  0   0   0   0   0   0   0   0   0   0   0   0   0

* TypSoil for sec# 1 (through ambient) [-]:
  3   3   3   3   3   3   3   3   3   3   3   3
  0   2   2   2   2   2   2   2   2   2   2   2   0
  0   2   2   2   2   2   2   2   2   2   2   2   0
  0   2   2   2   2   2   2   2   2   2   2   2   0
  0   2   2   2   2   2   2   2   2   2   2   2   0
  0   2   2   2   2   2   2   2   2   2   2   2   0
  0   2   2   2   2   2   2   2   2   2   2   2   0
  0   2   2   2   2   2   2   2   2   2   2   2   0
  0   0   0   0   0   0   0   0   0   0   0   0   0

* TypSoil for sec# 2 (through both zones) [-]:
  3   3   1   1   1   1   1   1   1   1   1   1
  0   2   2   1   1   1   1   1   1   1   1   1   0
  0   2   2   1   0   1   1   1   0   1   1   1   0
  0   2   2   1   1   1   1   1   1   1   1   1   0

```

TYPE 460 : HYPOCAUST (AIR-SOIL EXCHANGER)

0	2	2	1	1	1	0	1	1	1	0	1	1	0
0	2	2	1	1	1	1	1	1	1	1	1	1	0
0	2	2	1	0	1	1	1	0	1	1	1	0	0
0	2	2	1	1	1	1	1	1	1	1	1	1	0
	0	0	0	0	0	0	0	0	0	0	0	0	0
* TypSoil for sec# 3 (through setpoint-zone only) [-]:													
	3	3	2	2	2	2	2	2	2	2	2	2	
0	2	2	1	1	1	1	1	1	1	1	1	1	0
0	2	2	1	0	1	1	1	0	1	1	1	0	0
0	2	2	1	1	1	1	1	1	1	1	1	1	0
0	2	2	1	1	1	0	1	1	1	0	1	1	0
0	2	2	1	1	1	1	1	1	1	1	1	1	0
0	2	2	1	0	1	1	1	0	1	1	1	0	0
0	2	2	1	1	1	1	1	1	1	1	1	1	0
	0	0	0	0	0	0	0	0	0	0	0	0	0
* TypSoil for rear surface [-]:													
	0	0	0	0	0	0	0	0	0	0	0	0	0
	0	0	0	0	0	0	0	0	0	0	0	0	0
	0	0	0	0	0	0	0	0	0	0	0	0	0
	0	0	0	0	0	0	0	0	0	0	0	0	0
	0	0	0	0	0	0	0	0	0	0	0	0	0
	0	0	0	0	0	0	0	0	0	0	0	0	0
	0	0	0	0	0	0	0	0	0	0	0	0	0
* PosInf [-]:													
	1	1	1	9	12	7							
* Kair0 [kJ/K m2] ,Kair1 [(kJ/K m2)/(m/s)]:													
	0.1800E+02	0.1400E+02											
* LamSoil [kJ/K m], CvSoil [kJ/K m3]:													
	0.7200E+01	0.1000E+04											
	0.5400E+01	0.1000E+04											
* LamTub [kJ/K m], CvTub [kJ/K m3]:													
	0.7200E+01	0.1000E+04											
* ThTub [m], CtubCor [-], Cfric [-]:													
	5.0000E-03	0.8862E+00	2.0000E-02										
* TypWatFlow [-], Vwat [m/h]:													
	1	1	1										
	0.0000E+00	0.0000E+00	0.0000E+00										
* NiniSoil,NiniWat [-]:													
	2	1											
* TiniSoil [°C], PosIniSoil [-]:													
	0.1500E+02												
	0.1000E+02	3	3	1	11	12	7						
* ThIniWat [m], PosIniWat [-]:													
	0.0000E+00												
* Nopt [-]:													
	17												

TYPE 460 : HYPOCAUST (AIR-SOIL EXCHANGER)

```

* TypOpt [-], PosOpt [-]:
107  3  3  1  5 12  1 !Pfree#
107  6  3  1 11 12  1 !Pfix#
103  3  3  1  3 12  7 !Pfront
104 11  3  1 11 12  7 !Pback
105  3  3  1 11  3  7 !Pside
202  1  1  1  1  1  1 !Pwat
203  1  1  1  1  1  1 !Pfric
204  1  1  1  1  1  1 !Pin
 22  3  3  1 11 12  7 !PinHt
109  3  3  1 11 12  7 !PinHs
  5  3  3  1 11 12  7 !Mwat
  6  3  3  1 11 12  7 !dMlat
  9 11  3  1 11 12  7 !dMout
  1  4  3  1  4 12  7 !T1
  1  6  3  1  6 12  7 !T2
  1  8  3  1  8 12  7 !T3
  1 10  3  1 10 12  7 !T4
*****

```

Observations :

- Because of symmetry in the y-z plane, only half of the hypocaust has to be simulated, cutting middle two pipes by half ($N_{mod} = 2$ and last node width D_y is half the width of other ones).
- 3 cross-sections must be defined, one outside the building, two through the building (one cutting both zones, the other one through fixed zone only), as well as 3 surface conditions (ambient and floor of both zones).
- 2 temperature initialisation are used, for soils surrounding and beneath building respectively.

Building.bui : building definition file (Type 56)

```

*****
* TYPE 56 DESCRIPTION
*****

PROPERTIES
*****
DENSITY=1.204 : CAPACITY=1.012 : HVAPOR=2454 : SIGMA=2.041E-07
RTEMP =293.15

TYPES
*****

*-- LAYERS -----
LAYER Brick30
THICKNESS=.30 : CONDUCTIVITY=3 : CAPACITY=1 : DENSITY=1800

LAYER Insul10
THICKNESS=.10 : CONDUCTIVITY=0.144 : CAPACITY=0.72 : DENSITY=90

LAYER Soil40
THICKNESS=.40 : CONDUCTIVITY=7.2 : CAPACITY=1 : DENSITY=1000

*-- INPUTS -----

```

TYPE 460 : HYPOCAUST (AIR-SOIL EXCHANGER)

```

INPUTS TgFree TgFix

*-- WALLS -----
WALL Brick
LAYERS Brick30
ABS-FRONT=.8 : ABS-BACK=.8 : HFRONT=15 : HBACK=15

WALL Insul_Brick
LAYERS Insul10 Brick30
ABS-FRONT=.8 : ABS-BACK=.8 : HFRONT=15 : HBACK=15

WALL Soil
LAYERS Soil40
ABS-FRONT=.8 : ABS-BACK=0 : HFRONT=15 : HBACK=36
* rem : HBACK must be equal to Kbord from Type 460 *

WALL Insul_Soil
LAYERS Insul10 Soil40
ABS-FRONT=.8 : ABS-BACK=0 : HFRONT=15 : HBACK=36
* rem : HBACK must be equal to Kbord from Type 460 *

*-- COOLING -----
COOLING CoolFix
ON=15 : POWER=1E6 : HUMIDITY=0

*-- ORIENTATIONS -----
ORIENTATIONS Ambient

*-- ZONES -----
ZONES Free Fix

BUILDING
*****

*-- ZONE Free -----
ZONE Free

WALL=Insul_Brick : AREA=16 : ADJACENT=Fix : BACK : COUPLING=0
WALL=Brick : AREA=16 : EXTERNAL : ORIENTATION=Ambient : FSKY=0.5
WALL=Soil : AREA=8 : BOUNDARY=INPUT TgFree : COUPLING=0

REGIME
CAPACITANCE=1E+3 : VOLUME=16 : TINITIAL=15 : PHIINITIAL=50.0 : WCAPR=1

*-- ZONE Fix -----
ZONE Fix

WALL=Insul_Brick : AREA=16 : ADJACENT=Free : FRONT : COUPLING=0
WALL=Insul_Brick : AREA=41 : EXTERNAL : ORIENTATION=Ambient : FSKY=0.5
WALL=Insul_Soil : AREA=12 : BOUNDARY=INPUT TgFix : COUPLING=0

REGIME
COOL=CoolFix
CAPACITANCE=1E+3 : VOLUME=39 : TINITIAL=15 : PHIINITIAL=50.0 : WCAPR=1

```

TYPE 460 : HYPOCAUST (AIR-SOIL EXCHANGER)

```

OUTPUTS
*****

*-- TRANSFER -----
TRANSFER : TIMEBASE=1

*-- OUTPUTS -----

ZONES=Free
NTYPES=1 20

ZONES=Fix
NTYPES=1 20

END
*****

```

Observations :

- Preceding file must be processed by BID program before it can be used by Type 56 (for more details refer to Type56 component description).
- Note that for proper coupling with Type 460 *HBACK* of soil is set to identical value as *Kbord* from hypocaust and ground areas are identical to *Ssurf* from hypocaust (see Parameter control file to check this).

Type460.dck : simulation deck file

```

*****
* SIMULATION:
*****

*-----
ASSIGN  Trnsys.txt      6
ASSIGN  Out1.txt       101
ASSIGN  Out2.txt       102
ASSIGN  Out3.txt       103
ASSIGN  Type460.par    200
ASSIGN  Type460.con    201
ASSIGN  Building.bld  300
ASSIGN  Building.trn  301
ASSIGN  Building.win  302
*-----

*-----
EQUATIONS 37
*-----
DtSim   = 1
Tamb    = 30
Hamb    = 50
Aflow   = 1000
*-----
Tfree   = [1,1]
Tfix    = [1,5]

```

TYPE 460 : HYPOCAUST (AIR-SOIL EXCHANGER)

```

Pfree = -[1,4]
Pfix  = -[1,8]
*-----
Tout  = [2,1]
Psbl  = [2,3]
Plat  = [2,4]
TgFree = [2,5]
TgFix  = [2,6]
Pamb  = [2,7]
Pfree# = [2,11]
Pfix#  = [2,12]
Pfront = [2,13]
Pback  = [2,14]
Pside  = [2,15]
Pwat   = [2,16]
Pfric  = [2,17]
Pin    = [2,18]
PinHt  = [2,19]
PinHs  = [2,20]
Mwat   = [2,21]*1000
dMlat  = [2,22]*1000
dMout  = [2,23]*1000
T1     = [2,24]
T2     = [2,25]
T3     = [2,26]
T4     = [2,27]
*-----
PinH   = PinHt+PinHs
PinG   = Pin-PinHt-PinHs
PinH#  = Psbl+Plat+Pfree+Pfix+Pfront+Pback+Pside+Pwat
PinG#  = Pamb-Pfront-Pback-Pside
dMwat  = dMlat-dMout
Mwat#  = GT(TIME,1)*[3,1]+LT(TIME,2)*dMwat
* Mwat# = [3,1] replaced by preceding line because of bug in
*       integrator Type55
*=====

*=====
SIMULATION      1          100          DtSim
TOLERANCES     -0.0001    -0.0001
*=====

*****
* COMPONENTS:
*****

*=====
* Multizone Building
*-----
UNIT 1      TYPE 56

PARAMETERS 5
*-----
* 01) Logical unit of building description file
* 02) Logical unit of transfer coefficient file
* 03) Logical unit of window library file
* 04) Mode of calculation for star network
* 05) Weighting factor for operative romm temperature

```

TYPE 460 : HYPOCAUST (AIR-SOIL EXCHANGER)

```

300          301          302          0          0.5

INPUTS 8
*-----
* 01) Ambient temperature [°C]
* 02) Ambient humidity ratio [kg water / kg air]
* 03) Fictive sky temperature [°C]
* 04) Incident radiation for orientation ambient [kJ/hr]
* 05) Incident beam radiation for orientation ambient [kJ/hr]
* 06) Incident angle for orientation ambient [deg]
* 07) Ground temperature zone "Free" [deg C]
* 08) Ground temperature zone "Fix" [deg C]

Tamb        0,0          Tamb        0,0          0,0
0,0          TgFree      TgFix
0.000E+00   0.000E+00   0.000E+00   0.000E+00   0.000E+00
0.000E+00   0.100E+02   0.100E+02

* OUPUTS 8
*-----
* 01) Temperature of zone "Free" [°C]
* 02) Energy rate from zone "Free" to zone "Fix" [kJ/hr]
* 03) Energy rate from zone "Free" to "Ambient" [kJ/hr]
* 04) Energy rate from zone "Free" to "Ground" [kJ/hr]
* 05) Temperature of zone "Fix" [°C]
* 06) Energy rate from zone "Fix" to zone "Free" [kJ/hr]
* 07) Energy rate from zone "Fix" to "Ambient" [kJ/hr]
* 08) Energy rate from zone "Fix" to "Ground" [kJ/hr]
*=====
*=====
* Hypocaust
*-----

UNIT 2    TYPE 460

PARAMETERS 17
*-----
* 01) Logical unit parameter definition file
* 02) Logical unit parameter control file
* 03) Internal timestep [hr]
* 04) Minimum airflow [m3/hr]
* 05) Tolerance on tube temperature [K]
* 06-11) Surface types
* 12-17) Resistance at surface [K m2 hr/kJ]

2.000E+02   2.010E+02   0.000E+00   0.000E+00   1.000E-02
1.000E+00   1.000E+00   0.000E+00   0.000E+00   0.000E+00
0.000E+00   0.000E+00   0.000E+00   0.150E-01   0.000E+00
0.000E+00   0.000E+00

INPUTS 11
*-----
* 01) Air flow [m3/h]
* 02) Air inlet temperature [°C]
* 03) Air inlet humidity [%]
* 04) Air pressure [bar]

```


TYPE 460 : HYPOCAUST (AIR-SOIL EXCHANGER)

```

* 05) Water infiltration [m3/h]
* 06-11) Surface conditions [°C or W]

Aflow      Tamb      Hamb      0,0      0,0
Pfree      Pfix      Tamb      0,0      0,0
0,0

0.000E+00  0.000E+00  0.000E+00  1.000E+00  0.000E-03
0.000E+00  0.000E+00  Tamb      0.000E+00  0.000E+00
0.000E+00

* OUPUTS 30
*-----
* 01) Temperature of air outlet [°C]
* 02) Humidity of air outlet [%]
* 03) Sensible energy rate delivered to ground [kJ/hr]
* 04) Latent energy rate delivered to ground [kJ/hr]
* 05-10) Equivalent border conditions [°C or kJ/hr]
* 11-30) Optional outputs [fct of output type]
*=====

*=====
* Integrator
*-----
UNIT 3   TYPE 55
PARAMETERS 7
1 1 1 1 1E5 1 1E5
INPUTS 1
dMwat
0
*=====

*=====
* Printers
*-----
* PARAMETERS
*-----
* 01) Print time interval (>0=hours <0=months)
* 02) Time for start of printer (>0=hours <0=months)
* 03) Time for stop of printer (>0=hours <0=months)
* 04) Logical unit (<=0 for std Line Printer)
*-----
* Printer 1
UNIT 11  TYPE 25
*-----
PARAMETERS 4
1.000E+00  0.000E+00  1.000E+05  1.010E+02
INPUTS 10
Psbl      Plat      Pfree     Pfix      Pamb
Pfront    Pback    Pside     Pwat      Pfric
Psbl      Plat      Pfree     Pfix      Pamb
Pfront    Pback    Pside     Pwat      Pfric
*-----
* Printer 2
UNIT 12  TYPE 25
*-----
PARAMETERS 4
1.000E+00  0.000E+00  1.000E+05  1.020E+02

```

```

INPUTS 10
PinH      PinG      PinH#      PinG#      Pfree#
Pfix#     Mwat      Mwat#     dMlat     dMout
PinH      PinG      PinH#      PinG#      Pfree#
Pfix#     Mwat      Mwat#     dMlat     dMout
*-----
* Printer 3
UNIT 13   TYPE 25
*-----
PARAMETERS 4
1.000E+00  0.000E+00  1.000E+05  1.030E+02
INPUTS 10
Tfree     Tfix      TgFree     TgFix      Tamb
T1        T2        T3         T4         Tout
Tfree     Tfix      TgFree     TgFix      Tamb
T1        T2        T3         T4         Tout
*-----
*****
END
*****

```

Observations :

- Linking is done by feeding upper hypocaust surfaces with outflowing energy rates (*Pfree* and *Pfix*) from the two zones and reciprocally feeding building with upper border temperatures (*Tfree* and *Tfix*) from hypocaust.
- Internal energy gains of hypocaust (*PinH*, *PinH#*) and surrounding ground (*PinG*, *PinG#*) are each defined by two alternative ways, so as to check for proper energy balance. Same is done for total free water within tubes (*Mwat*, *Mwat#*) and energy diffused from zones to hypocaust (*Pfree*, *Pfree#*, *Pfix*, *Pfix#*).

Results of simulation

Parameters defined further up and printed in output files are plotted hereafter and show following, expected dynamic :

- Airflow heats up hypocaust (see Fig. 3, *Psbl*). During first hours, energy diffuses from building and surrounding soil into colder hypocaust and as latter warms up diffusion reverses (see Fig. 4, *Pfront*, *Pback*, *Pside*, *Pfree*, *Pfix*).
- As airflow heats up hypocaust it cools down along the tubes (see Fig. 2, stratification of *Tamb*, *T1-T4*, *Tout*) and with time tends to reach equilibrium temperature.
- Warm and humid airflow condenses during first hours (see Fig. 3, *Plat* and Fig. 5, *dMlat*, *Mlat*). As ground temperature rises, all free water within tubes then evaporates again, after which no latent exchanges take place any more.
- Within Type 460 energy balance is correct (see Fig. 3 *PinH*, *PinH#*, *PinG*, *PinG#*), as is mass balance (see Fig. 5, *Mwat*, *Mwat#*). Consistency of energy flows between modules is also respected (see Fig. 4, *Pfree*, *Pfree#*, *Pfix*, *Pfix#*).

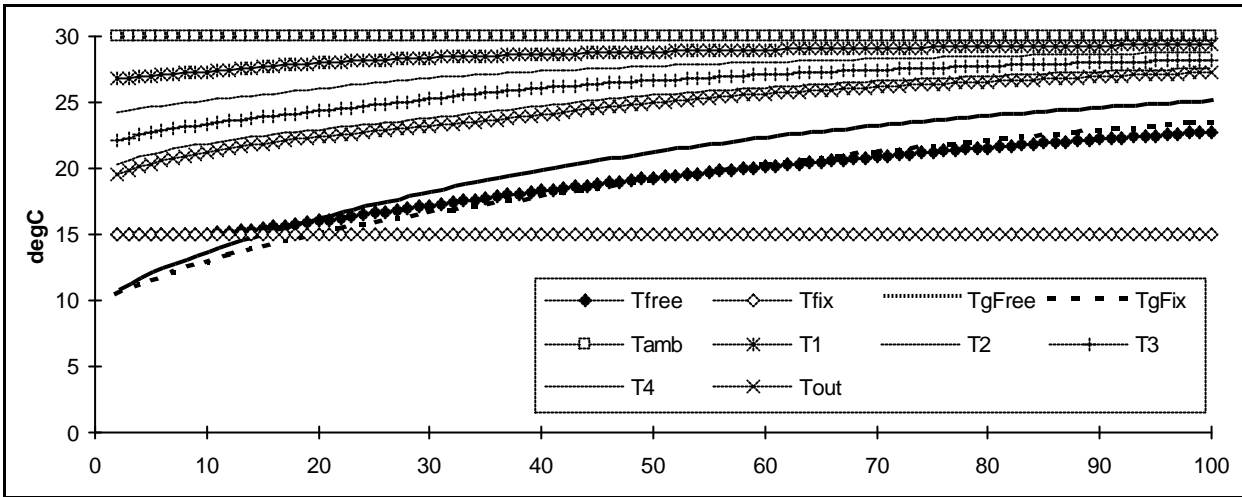


Fig. 2 : Temperature of air (T_{free} , T_{fix}) and ground (T_{gFree} , T_{gFix}) of both zones as well as of airflow along the tubes (T_1 - T_4) and at inlet and outlet (T_{amb} , T_{out}).

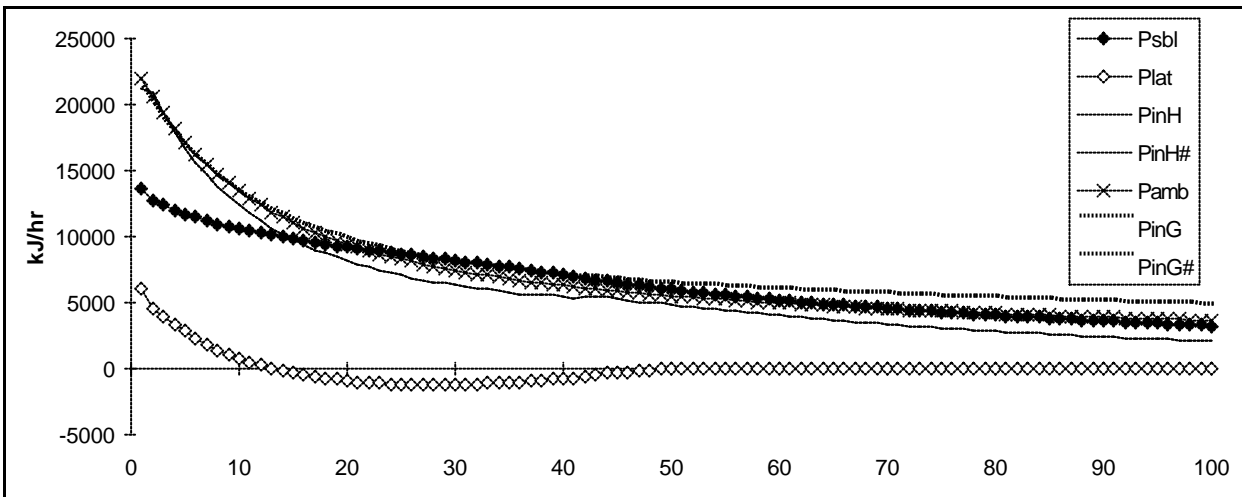


Fig. 3 : Internal heat gains of hypocaust (P_{inH} , $P_{inH\#}$) and surrounding soil (P_{inG} , $P_{inG\#}$), as well as energy entering hypocaust by airflow (P_{sbl} , P_{lat}) and diffused from ambient into surrounding soil (P_{amb}).

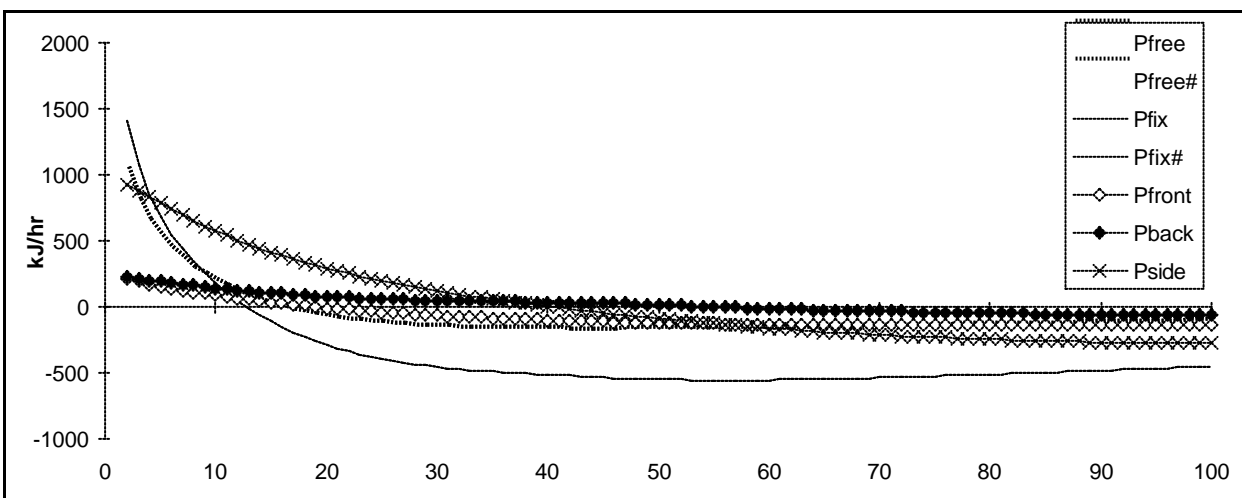


Fig. 4 : Energy entering hypocaust from building (P_{free} , $P_{free\#}$, P_{fix} , $P_{fix\#}$) and from surrounding soil (P_{front} , P_{back} , P_{side}).

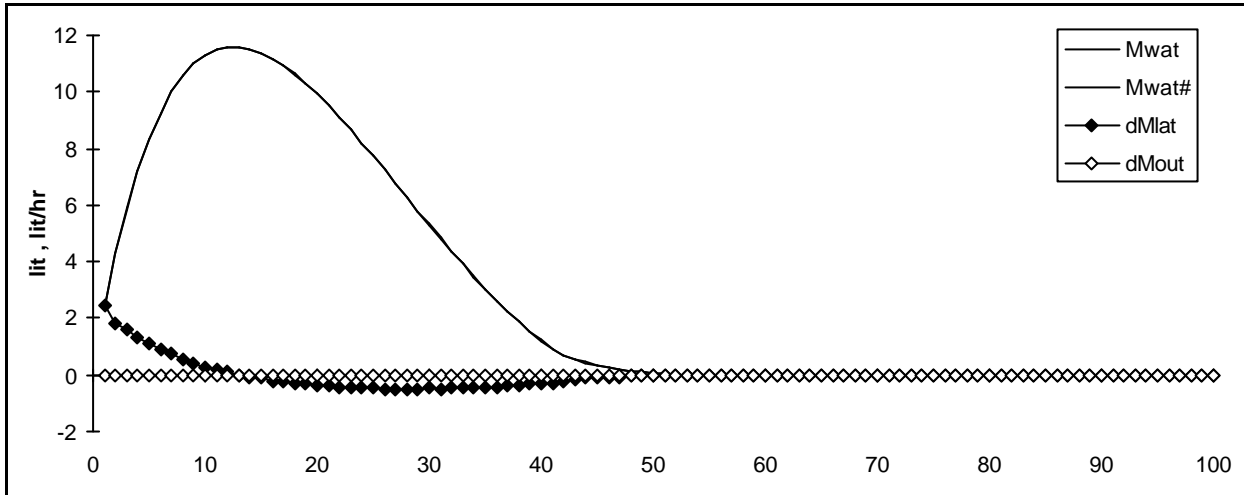


Fig. 5 : Free water in tubes (Mwat, Mwat#) as well as water condensation (dMlat) and flux out of tubes (dMout).